

# 汽车安全玻璃试验方法第 4 部分：太阳 能透射比测定方法

! " # \$ % & ' ( ) \* + , - . /

Road vehicles—Safety glazing materials—Method for determination of solar transmittance

01234567689: ; <

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2001-10-01 =>

1 ? @

ABCD- E ! " # \$ % F G H I J K L ! M N O P " # \$ % Q & ' R S T ) \* + U & ' ( V W ) \* + F & ' ( 9 ) \* + Q , - . / X

ABCYNZ ! " # \$ % F G H I J K L ! M N O P " # \$ % & ' ( ) \* + Q , - X

2 [ N B C

\ ] B C ^ \_ ` Q a b c d e f A B C g [ N h i j k A B C Q a b X A B C I m n c ^ o m A p k q r X ^ q B C s t u v w c x N A B C Q O . y z { x N \ ] B C | } m A Q ~ ( • X

GB/T 2680-1994 ! \$ % ~ " # ) \* + U & ' # V W ) \* + U & ' ( 9 ) \* + U R S T ) \* + F q \$ % \$ % & ' Q , - X

3 - (

A B C ) N \ ] - ( X

3.1 ) \* +

f \* - Q + , a - . # / a - \ c ) \* d 3 . O \* d 3 Q + 1 X

3.2 23234+15

6, 78&' 9: Q; 3238f BC; 3<\c=6, 7>f?@ABC &' DZ6, 7EB. nQ; 323Q+1X

3.3 &' (: W) \* +

u" # \$ % F G H I J c K L M \* O ! N Q ( 38G ^ H I Q &' ( M \* ( Q + 1

3.4 O P Q R A

O P Q R A 15D- E R S T M \* U V Q S T ? @ k 300nm U 400nm c 23 23k 1.5X

3.5 O P Q R B

O P Q R B 15D- E R S T M \* U V Q S T ? @ k 300nm U 380nm c 23 23k 1.0X

4 &' ( ) \* + Q , -

4.1 , 3 V W

X. / Y Z [ N \ q ] ^ \_ Q ` a ^ # b c d , 3 \$ % F G Q # / ) \* +

1 XG, 3?@g( he&' M\* i j \_k A Q I m S / ? @ 4 n o 300nm U  
2500nm 5 X

4.2 p q C r A e p ) N @ s e 7 t c u g n ~ v w x y s e 7 t Q | @ z  
{ D X N | } ~ • ! e " # \$ % & ' ( c u Y n ~ ) N G H Y N Z F G Q . /  
' ( e 7 t X

4.3 , - ) \*  
+ , ` a ^ # # b c - . T / Q Y Z O 7 V W X 1 O ' 2 e p c 3 x 9 8 4  
e Q # 5 6 V X 7 Y N c y B 8 e p 9 A + : A Q . ; c < = p q # / ) \* + 1 X

4.4 ' , > ?

4.4.1 @ O P Q R A c P

4.4.1.1 &' ( R S T M \* ) \* + T U V 4 4 0 0 5 A

[ N Q B 4 1 5 F C = A ( B C Q C = c 2 3 2 3 = 1.5 ) c D 3 0 0 n m U 4 0 0 n m c  
v 5 n m k E F : c E F : E F : j G H ) \* + 1 c I ] ^ c P J I &' ( R S  
T M \* ) \* + X

T U V 4 4 0 0 5 = ..... 4 1 5

B g A

K K f S T F : [ ] c N L M / c P J u v E Q &' ( X

4.4.1.2 &' ( V W ) \* + T D S 4 1.5 5 A

[ N Q B 4 2 5 . C = B D 3 0 0 n m U 2 5 0 0 n m 2 5 c ^ N v 5 n m U 1 0 n m U 5 0 n m  
k E F : c E F : E F : j G H ) \* + 1 c I ] ^ c P J I &' ( V W ) \* + X  
T U V 4 1.5 5 = ..... ( 2 )

B g A

K K f S T F : [ ] c N L M / c P J u v E Q &' ( X

4.4.2 @ O P Q R B c P

4.4.2.1 &' ( R S T M \* ) \* + T U V 4 3 8 0 5 A [ N Q B 4 3 5 . C = C ( B  
C Q C = c 2 3 2 3 = 1.0 ) D 3 0 0 n m U 3 8 0 n m c v 5 n m k E F : c E F : E F :  
Q G H ) \* + 1 c I ] ^ c P J I &' ( R S T M \* + X

T U V 4 3 8 0 5 = [ ] ..... ( 3 ) B g A

K K f S T F : [ ] c N L M / c P J u v E Q &' ( X

4.4.2.2 &' ( V W ) \* + T D S 4 1.0 5 A

[ N Q B 4 4 5 . C = D ( B C Q C = c 2 3 2 3 = 1.0 ) D 3 0 0 n m U 2 5 0 0 3 5 n m c  
^ N v 5 n m U 1 0 n m U 5 0 n m k E F : c E F : E F : j G H ) \* + 1 c I ] ^ c  
P J I &' ( V W ) \* + X ..... ( 4 ) B g A

K K f S T F : [ ] c N L M / c P J u v E Q &' ( X

4.4.3 &' ( 9 ) \* +

A B C D - E N O P Q R A . B , - " # \$ % F G &' ( V W ) \* + Q .  
/ X u Y n c ~ [ N 4.4.1.2 • 4.4.2.2 Q &' ( V W ) \* + , - O P . C = E 4 B  
C Q C = 5 g Q Q B d c P &' ( 9 ) \* + X

5 O P k Q

R S g y T U A e p V b U W s U O i X 7 P Y N c X \_ Y : A . ; Z x N  
V W F ^ [ N Q O P Q R 4 A • B 5 Z e p 9 U V . &' ( V W ) \* + c u Y n c  
X \_ Y e p Q &' ( 9 ) \* + c 3 \ ] n 0.1 % X

C = A

$$= 2323k 1.5ncuvEJ Q^{\$ \# / \wedge < \& ' ( [ ] 8STF : [ ] Q\_ ]$$

ST` 4nm5	[Ea b c ` ]
300	0.000000
305	0.001045
310	0.004634
315	0.011800
320	0.019807
325	0.027019
330	0.043271
335	0.042703
340	0.047644
345	0.048041
350	0.053948
355	0.054947
365	0.064930
370	0.072925
375	0.075901
380	0.077991
385	0.075890
390	0.073777
395	0.092335
400	0.055446
TUV(400)=d <sub>300</sub> <sup>400</sup> T` b [Ea b c ` ]	

$$C = B$$

$$= 2323k 1.5ncuvEJ Q^{\$ \# / \wedge < \& ' ( [ ] 8STF : [ ] Q\_ ]$$

ST` 4nm5	[Ea b c ` ]	ST` 4nm5	[Ea b c ` ]	ST` 4nm5	[Ea b c ` ]
300	0.000000	410	0.011712	850	0.049016
305	0.000048	420	0.011973	900	0.039872
310	0.000214	430	0.010839	950	0.016652
315	0.000545	440	0.013166	1000	0.037501
320	0.000915	450	0.015431	1050	0.034127
325	0.001248	460	0.016175	1100	0.020859
330	0.001999	470	0.015988	1150	0.012512
335	0.001973	480	0.016466	1200	0.021415
340	0.002201	490	0.015565	1250	0.023934
345	0.002219	500	0.015661	1300	0.018651
350	0.002446	510	0.016043	1350	0.001642
355	0.002538	520	0.015016	1400	0.000136

360	0.002630	530	0.015900	1450	0.003746
365	0.002999	540	0.015681	1500	0.009548
370	0.003369	550	0.015790	1550	0.013934
375	0.003506	560	0.015539	1600	0.012093
380	0.003603	570	0.015184	1650	0.011636
385	0.003506	580	0.014646	1700	0.010440

390 0.003408 590 0.014112 17.6 0.48 15.6 re fBT112.56 692.88 TD (3

310	0.000606	430	0.012238	950	0.018065
315	0.001181	440	0.014670	1000	0.033953
320	0.001714	450	0.016974	1050	0.030606
325	0.002133	460	0.017279	1100	0.020713
330	0.003018	470	0.016900	1150	0.011434
335	0.002868	480	0.017266	1200	0.020192
340	0.003107	490	0.016186	1250	0.021564
345	0.003060	500	0.016186	1300	0.017439
350	0.003307	510	0.016483	1350	0.002378
355	0.003372	520	0.015351	1400	0.000279
360	0.003437	530	0.016203	1450	0.004445
365	0.003857	540	0.015918	1500	0.009458
370	0.004278	550	0.015982	1550	0.012435
375	0.004385	560	0.015581	1600	0.010940
380	0.004463	570	0.015133	1650	0.010588
385	0.004438	580	0.014168	1750	0.007222
390	0.004412	600	0.014414	1800	0.001912
395	0.005246	610	0.014659	1850	0.000348
400	0.009117	620	0.014379	1900	0.000000
		630	0.014099	1950	0.000892
		640	0.013966	2000	0.002044
		650	0.013833	2050	0.003782
		660	0.013624	2100	0.004029
		670	0.013363	2150	0.003659
		680	0.012234	2200	0.003224
		690	0.011111	2250	0.003151
		700	0.011826	2300	0.003028
		710	0.012536	2350	0.002858
		720	0.010445	2400	0.002231
		730	0.010972	2450	0.001116
		740	0.011707	2500	0.000000
		750	0.011484		
		760	0.009045		
		770	0.010192		
		780	0.010732		
		790	0.010526		
		800	0.010526		

TUV 44005 =  $d_{300}^{400} T^{-b} [E a b c^{-}]$